

TRANSPARENT HIGH IMPACT ALLOY

BACKGROUND OF THE INVENTION

1. Field of the Invention

The invention relates to a polymer alloy
5 comprising a brittle polymer and either a ductile polymer, a rubbery polymer, or a ductile polymer and a rubbery polymer. More particularly, the invention pertains to a polymer alloy comprising at least a brittle polymer component having a weight average
10 molecular weight greater than 180,000 and a plasticizer in an amount greater than 0.4 weight percent. The polymer alloy gives improved toughness with excellent transparency and/or improved low haze with improved toughness and stiffness.

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2. Background Art

It is known in the art that some physical properties of styrenic or acrylic type polymers may be improved by alloying them with one or more
20 additional polymers. In some cases, the resulting mixture can have improved mechanical properties, such as improved impact strength or toughness. However, as impact strength or toughness is improved, the stiffness of the alloy usually is
25 decreased.

Chemical Abstracts 109:171278v [Polym. Prepr.
(Am. Chem. Soc., Div. Polym. Chem.) 1988, 29(2),
180-1] discloses that physical blends of block SBR
(styrene content: 75.2 weight percent) and a
30 copolymer of methyl methacrylate and styrene are
mechanical properties of the blend are partially compatible. The morphological and mechanical

properties of the blend are strongly dependent on the molding/mixing process used to produce the blend. The SBR could only be toughened when the ideal morphology of the blend was obtained.

5 Chemical Abstracts 106:85901z [JP 61/200,151] discloses thermoplastic compositions comprising from 5 to 95 weight percent of a block copolymer and from 95 to 5 weight percent of a thermoplastic polymer (e.g. ABS). The block copolymer is derived from
10 coupling an aromatic vinyl polymer block with an aromatic vinyl monomer-conjugated diene copolymer block. The subject thermoplastic compositions apparently have improved impact strength.

Chemical Abstracts 112:8285y [JP 61/291,610]
15 discloses the use of "impact modifiers" for thermoplastic polymers. The modifiers are basically similar to the block copolymer disclosed by Chemical Abstracts 106:85901z.

Chemical Abstracts 99:196070j [JP 58/122,954]
20 discloses improvement of anisotropy of a styrene hydrocarbon-conjugated diene block copolymer by blending it with a styrene-methacrylic ester copolymer. Such a blend, when extruded to form a molded plate, apparently possesses superior physical
25 properties.

Chemical Abstracts 111:8522c [JP 01/45614] discloses high-impact styrene polymer compositions comprising a major amount of a styrene (50 to 90 weight percent)-conjugated diene (50 to 10 weight
30 percent) block copolymer and a minor amount of a styrene-based polymer (e.g. styrene-methyl methacrylate copolymer).

U.S. Patent No. 5,290,862, assigned to the same

assignee as that of the present invention, discloses a polymer alloy comprising (i) from 30 to 82 weight percent of a brittle polymer; (ii) from 3 to 50 weight percent of a rubbery polymer; and (iii) from 5 15 to 67 weight percent of a ductile polymer which is compatible with the rubbery polymer. The polymer alloy possesses a combination of improved properties, including improved impact strength. Typically these alloys have a Notched IZOD impact 10 strength of greater than 0.5 foot pound/inch, preferably greater than 1.0 foot pound/inch, and may have a haze of less than 10, most preferably less than 5. The brittle polymer generally may have a molecular weight of about 220,000.

15 Even though the polymer alloy of the above U.S. Patent No. 5,290,862 is adequate for certain end use applications, such as patio tumblers, requiring extremely low haze and good impact resistance, some critical applications may require a polymer alloy 20 material with improved low haze with improved toughness and stiffness and/or improved toughness with excellent transparency.

SUMMARY OF THE INVENTION

25 The invention has met the above need. The invention provides an improved tough and transparent polymer alloy comprising:

from 90 to 20 weight percent of a brittle polymer;

30 from 0 to 60 weight percent of a rubbery polymer; and

from 0 to 80 weight percent of a ductile

polymer whereby the ductile polymer and the rubbery polymer are compatible; and

greater than 0.4 weight percent of a plasticizer.

- 5 The brittle polymer has a weight average molecular weight greater than 180,000. In a first embodiment, the weight average molecular weight is greater than 220,000, preferably ranging between 270,000 and 300,000, and most preferably is 280,000.
- 10 In a second embodiment of the invention, the weight average molecular weight ranges between about 190,000 and 300,000; and preferably ranges between 195,000 and 270,000. Both the first and the second embodiments comprise the brittle polymer and the
- 15 plasticizer and either the rubbery polymer or the ductile polymer or both.

The polymer alloy of the first embodiment is comprised of from about 80 to 20 weight percent, preferably from about 70 to about 40 weight percent, and most preferably, about 50 to about 55 weight percent of the brittle polymer; from 0 to about 3 weight percent, and more preferably, 0 weight percent of the rubbery polymer; from about 20 to 80 weight percent, preferably from about 30 to 60 weight percent, and most preferably about 50 to about 45 weight percent of the ductile polymer; and from about 0.5 to about 3.0 weight percent, preferably from about 1 to about 2 weight percent, and most preferably about 1.5 weight percent of plasticizer.

The polymer alloy of the second embodiment is comprised of from about 80 to 20 weight percent, preferably from about 70 to 50 weight percent, and

most preferably, from about 65 to about 55 weight percent of the brittle polymer; from about 5 to about 60 weight percent, preferably from about 5 to about 20 weight percent, and most preferably from 5 about 8 to about 12 weight percent of the rubbery polymer; from about 0 to about 60 weight percent, more preferably from about 20 to about 40 weight percent; and most preferably from about 25 to about 35 weight percent of the ductile polymer; and 10 greater than 0.4 weight percent, more preferably from about 0.5 to about 3.0 weight percent, and most preferably from about 0.7 to about 1.5 weight percent of the plasticizer.

The brittle polymer preferably is a copolymer 15 of a styrene and methyl methacrylate and preferably, the plasticizer is mineral oil. The plasticizer can be part of any one of the polymers comprising the polymer alloy or it can be blended along with the polymers to form the polymer alloy of the invention.

20 Preferably, the plasticizer is part of the brittle polymer and resides in the brittle polymer prior to the brittle polymer being blended with the other polymer components of the polymer alloy of the invention.

25 The ductile polymer preferably is a styrene butadiene block copolymer and may be present in the polymer alloy in an amount ranging from about 30 to about 60 weight percent. Preferably, the butadiene is present in this styrene butadiene block copolymer 30 in an amount ranging between 20 to 35 weight percent, preferably from about 24 to about 26 weight percent, and more preferably, about 25 weight percent.

The rubbery polymer preferably is a styrene butadiene block copolymer having 55 to 70 weight percent butadiene.

- The polymer alloys of the invention have
- 5 improved low haze with improved toughness and stiffness and/or improved toughness with excellent transparency. For the first embodiment, when the indices of refraction of the different phases of the polymer alloy formed by the polymers and the
- 10 plasticizer are matched within a + or - 0.005, the haze will be less than 5%; when matched within a + or - 0.002 the haze will be less than 3%, and more preferably the haze will be less than 1.5%. For the second embodiment, when the indices of refraction of
- 15 the different phases of the polymer alloy formed by the polymers and the plasticizer are matched within a + or - 0.005, the haze will be less than 10%; when matched within a + or - 0.002 the haze will be between 1% and 4%.
- 20 The polymer alloy of the invention has a Notched IZOD impact strength ranging between about 1.0 to about 6.0, and preferably, ranging between about 2.0 and 4.5 foot pound per inch measured according to ASTM D-256.
- 25 These and other objects of the invention will be better appreciated and understood by those skilled in the art from the following description and appended claims.

30 DETAILED DESCRIPTION OF THE INVENTION

The polymer alloy of the present invention is an improvement of the polymer alloy described and claimed in the aforesaid U.S. Patent No. 5,290,862,

the teachings of which are incorporated herein by reference.

As used in this specification, the term "brittle" means a polymer having an elongation at break up to 15%, preferably less than 10%, as measured by ASTM D-638. The term "ductile" means a polymer having an elongation at break greater than 15%, as measured by ASTM D-638. The term "rubbery" means a natural or synthetic polymer, which at room temperature can be stretched to at least twice its original length, and upon immediate release of the stress, will return to its approximate original length. The term "compatible" means two or more polymers that have good interfacial adhesion (for example, the blended polymers exhibit physical properties approximating those expected from the rule of mixtures). The term "miscible" means two or more polymers which, when blended form a single phase that remains clear, even if the refractive indices of the polymers do not match.

The polymer alloy of the invention is comprised generally of a brittle polymer with a weight average molecular weight greater than 180,000; a rubbery polymer; and/or a ductile polymer; and a plasticizer in an amount greater than 0.4 weight % based on the total weight of the polymer alloy and preferably residing in the brittle polymer.

The brittle polymer used in the improved polymer alloy of the invention may be selected from the group of polymers consisting of polymers comprising:

(i) from 80 to 45 weight percent of one or more C₈₋₁₂ vinyl aromatic monomers which are unsubstituted

or substituted by a C₁₋₄ alkyl radical;

(ii) from 20 to 55, weight percent of one or more C₁₋₆ alkyl esters of C₃₋₆ ethylenically unsaturated carboxylic acids; and

5 (iii) from 0 to 5 weight percent of one or more C₃₋₆ ethylenically unsaturated carboxylic acids or anhydrides.

The C₈₋₁₂ vinyl aromatic monomer suitable for use in the brittle polymer component is not particularly 10 restricted and may be unsubstituted or substituted by a C₁₋₄ alkyl radical. Preferably, the C₈₋₁₂ vinyl aromatic monomer is selected from the group comprising styrene, α-methyl styrene, p-methyl styrene and t-butyl styrene. The preferred C₈₋₁₂ vinyl 15 aromatic monomer is styrene.

The choice of C₁₋₆ alkyl ester of a C₃₋₆ ethylenically unsaturated carboxylic acid for use in producing the brittle polymer is not particularly restricted. Non-limiting suitable examples of alkyl 20 esters include acrylic ester, methyl methacrylate, methyl acrylate, ethyl acrylate, ethyl methacrylate, butyl acrylate and butyl methacrylate. The preferred alkyl ester is methyl methacrylate.

A brittle polymer suitable for use in the 25 polymer alloy of the invention is a copolymer of styrene and methyl methacrylate (SMMA). Preferably, such a copolymer comprises from about 80 to about 45 weight percent, preferably from about 80 to about 65 weight percent, styrene, and from about 20 to about 30 55 weight percent, preferably from about 20 to about 35 weight percent, methyl methacrylate (MMA). Such a copolymer is commercially available from NOVA Chemicals Inc. under the trademark NAS 90.

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The production of a brittle polymer suitable for use in the polymer alloy of the present invention is within the purview of a person skilled in the art. Such polymers may be produced by
5 suspension, solution, emulsion, or bulk polymerization. This brittle polymer may be made in a reactor in which the plasticizer, especially if mineral oil, can also be added.

The brittle polymer suitable for use in the
10 polymer alloy of the present invention has a weight average molecular weight greater than 180,000. In a first embodiment, the weight average molecular weight of the brittle polymer is greater than 220,000, preferably between about 270,000 to about
15 300,000, and most preferably about 280,000. In the second embodiment, the weight average molecular weight of the brittle polymer is greater than 180,000, preferably between about 190,000 and 300,000, and most preferably between about 195,000
20 and 270,000. In some end-use applications, the weight average molecular weight may be as high as 400,000.

The method for producing a polymer alloy with molecular weights of this magnitude are well known
25 to those skilled in the art. For example, a desired molecular weight can be obtained by varying the conditions of the reactor in which the brittle polymer is polymerized, i.e. temperature, amount and type of initiator, and the type of polymerization
30 process.

The inventors have found that by increasing the weight average molecular weight of the brittle polymer, and by adding a plasticizer, such as

100-200-44-100-200

mineral oil, to the polymer alloy of the invention, very little or no rubbery polymer or ductile polymer may be needed in the polymer alloy in order to provide a tough, transparent high impact alloy with
5 an acceptable Notched IZOD value and with very little haze. More specifically, the inventors have found that the combination of increasing the weight average molecular weight of the brittle polymer and adding the plasticizer to the polymer alloy
10 increases 1) the efficiency of the rubbery and/or ductile components and 2) the toughness of the polymer alloy when compared to only increasing the molecular weight of the brittle polymer. This improved efficiency of the rubbery and ductile
15 polymers allows lower amounts of these components to be used in the polymer alloy of the invention or allows one of these components to be eliminated from the polymer alloy of the invention. Thus, the negative effects which are usually associated with
20 high amounts of these two components, which relate to "haze" and/or "stiffness" of the polymer alloy are lessened or decreased.

In a broad aspect of the invention, the brittle polymer is used in the polymer alloy in an amount
25 from 90 to 20 weight percent, based on the total weight of the polymer alloy. In the first embodiment, this amount will range from about 80 to 20 weight percent, more preferably from about 70 to 40 weight percent, and most preferably, from about
30 50 to about 55 weight percent, based on the total weight of the polymer alloy, and the weight average molecular weight is greater than 220,000, more

preferably between 270,000 and 300,000, and most preferably, is about 280,000.

In the second embodiment, the amount of brittle polymer ranges between about 80 to 20 weight percent, more preferably, 70 to 50 weight percent, and most preferably, from about 65 to about 55 weight percent, based on the total weight of the polymer alloy, and the weight average molecular weight is greater than 180,000, more preferably is 10 between about 190,000 and 300,000, and most preferably, ranges between about 195,000 and 270,000.

Preferably, the ductile polymer of the polymer alloy ranges between about 0 to about 80 weight percent. This ductile polymer preferably is derived from 65 to 80 weight percent of one or more C₈₋₁₂ vinyl aromatic monomers; and 35 to 20 weight percent of one or more C₄₋₆ conjugated diolefins.

A ductile polymer suitable for use in the polymer alloy of the present invention is a tapered, linear or radial di-block (vinyl aromatic monomer-conjugated diene) or tri-block (vinyl aromatic monomer-conjugated diene-vinyl aromatic monomer) copolymer. The production of such copolymers is known to those skilled in the art. Such polymers can be produced by living solution polymerization (e.g. using a lithium catalyst). Examples of suitable ductile polymers for use in the present invention are available from Chevron-Phillips, Kraton, and AtoFina.

In the first embodiment, the ductile polymer of the polymer alloy ranges from between 20 to 80 weight percent, preferably from between 30 to 60

weight percent, and most preferably, is about 45 to 50 weight percent. In the second embodiment, the ductile polymer of the polymer alloy ranges between 0 to 60 weight percent, preferably between 20 to 40 weight percent, and most preferably ranges between 25 to 35 weight percent.

The rubbery polymer of the polymer alloy broadly ranges between about 0 to about 60 weight percent based on the total weight of the polymer alloy. This rubbery polymer preferably is derived from 30 to 45 weight percent of one or more C₈₋₁₂ vinyl aromatic monomers and from 70 to 55 weight percent of one or more C₄₋₆ conjugated diolefins.

A rubbery polymer suitable for use in the present polymer alloy may be a linear, tapered, or radial di-block (aromatic vinyl monomer-conjugated diene) or a tri-block copolymer (vinyl aromatic monomer-conjugated diene-vinyl aromatic monomer). As is known in the art, a tapered di-block copolymer is a copolymer comprising a block which becomes progressively rich in one of the constituent monomers in a segment (typically, the end) of the block.

The process by which such a tapered copolymer
is obtained is similar to the process by which block
copolymers are obtained except that there is an
incremental adjustment in the monomer feed (e.g.
richer or poorer in vinyl aromatic/conjugate
diolefin) to produce a block polymer which is
"tapered". Examples of suitable rubbery polymers
for use in the present polymer alloys are
commercially available from Ato-Fina, Dexco

Polymers, and Firestone Synthetic Rubber and Latex Company.

In the first embodiment, the amount of rubbery polymer more preferably, ranges from about 0 to 5 about 3 weight percent, most preferably, 0 weight percent, based on the total weight of the polymer alloy. In the second embodiment, the amount of rubbery polymer ranges from about 5 to about 60 weight percent, more preferably, from about 5 to 10 about 20 weight percent, and most preferably, from about 8 to 12 weight percent, based on the total weight of the polymer alloy.

Suitable C₈₋₁₂ vinyl aromatic monomers for use in the ductile polymer and the rubbery polymer of 15 the present invention are not particularly restricted and may be unsubstituted or substituted by a C₁₋₄ alkyl radical. Preferably, the C₈₋₁₂ vinyl aromatic monomer is selected from the group comprising styrene, α-methyl styrene, p-methyl 20 styrene and t-butyl styrene. A preferred C₈₋₁₂ vinyl aromatic monomer is styrene. Generally, the ductile polymer will contain a larger amount of vinyl aromatic monomer, typically in the range from 65 to 80 weight percent; and the rubbery polymer will 25 contain lower amounts of vinyl aromatic monomer, typically in the range 30 to 45 weight percent.

The C₄₋₆ conjugated diolefin suitable for use in the ductile polymer and the rubbery polymer of the polymer alloy of the present invention is not 30 particularly restricted and may be unsubstituted or substituted by a chlorine atom. Preferably, the C₄₋₆ conjugated diolefin is selected from the group comprising 1,3-butadiene and isoprene. The preferred

diolefin, particularly for the ductile polymer is butadiene. Thus, the preferred ductile polymer is a styrene butadiene block copolymer. The preferred diolefin particularly for the rubbery polymer is
5 butadiene, and thus the preferred rubbery polymer is a styrene butadiene block copolymer. Generally, the amount of the C₄₋₆ conjugated diolefin in the rubbery polymer will range from about 55 to about 70 weight percent based on the total weight of the rubbery
10 polymer. The amount of the C₄₋₆ conjugated diolefin in the ductile polymer will range from about 20 to about 35 weight percent, based on the total weight of the ductile polymer.

If a rubbery polymer and the ductile polymer
15 are both used in the polymer alloy of the present invention, then the rubbery and ductile polymers should at least be compatible. Preferably, the polymers will be miscible, as defined herein.

The plasticizer is used in the polymer alloy of
20 the invention in an amount greater than 0.4 weight percent based on the total weight of the polymer alloy. More specifically, the amount of plasticizer used in the polymer alloy of the first embodiment will range from about 0.5 to about 3.0 weight
25 percent, more preferably between about 1.0 to about 2.0 weight percent, and most preferably, about 1.5 weight percent. The amount of plasticizer used in the polymer alloy of the second embodiment will be greater than 0.4, preferably from about 0.5 to about
30 3.0 weight percent, most preferably between about 0.7 to about 1.5 weight percent.

The plasticizer is not particularly limited and a suitable plasticizer may be selected from

conventional plasticizers used for thermoplastic acrylic resins as taught in U.S. Patent No. 6,280,835. For example, plasticizers having good compatibility with the brittle polymer, the rubbery polymer, and the ductile polymer of the invention can be used. Examples of such plasticizers include alkyl benzyl phthalates, such as octyl benzyl phthalate and myristyl benzyl phthalate; dialkyl phthalates, such as dibutyl phthalate, dihexyl phthalate, and dioctyl phthalate; esters of phosphoric acid, such as tricresyl phosphate and trioctyl phosphate; esters of fatty acids, such as dibutyl sebacate and acetyl tributyl citrate; polyesters, such as polyesters derived from adipic acid, polyesters derived from sebacic acid, and polyesters derived from phthalic acid; derivatives of glycols, such as diethylene glycol dibenzoate, dipropylene glycol dibenzoate, and triethylene glycol di(2-ethylhexoate); derivatives of glycerol, such as glycerol triacetate and glycerol tributyrate; and epoxy derivatives, such as epoxidized soy bean oil.

The plasticizer may be selected from the group consisting of mineral oil, vegetable oil, animal oil, synthetic oil, silicone oil, and fluorinated oil. Preferably, the plasticizer used in the invention is mineral oil.

The plasticizer can be part of any one of the polymers comprising the polymer alloy or it can be blended along with the polymers to form the polymer alloy of the invention. That is, the plasticizer can be added to any of the polymers during its production or it can be compounded into any of the

polymers in a separate step or it can be compounded along with the polymers during the production of the polymer alloy of the invention or it can be added using a combination of these methods. Preferably,
5 the plasticizer is blended with the brittle polymer, more preferably the plasticizer is added during the production of the brittle polymer, and preferably, the plasticizer resides in the brittle polymer when the brittle polymer is added to or compounded with
10 the rubbery polymer and/or the ductile polymer to form the polymer alloy.

The rubbery and ductile phases are at least compatible. That is, these components of the polymer alloy of the invention will have good interfacial adhesion. Under stress they will not delaminate.
15 Preferably, the rubbery and ductile components are miscible. That is, when blended they will form a clear component, whether or not their refractive indices are matched or close.

20 The components of the polymer alloy, i.e. the brittle polymer, the rubbery polymer, the ductile polymer and the plasticizer, constitute different phases within the polymer alloy. Preferably, only two different phases will be formed. The amounts
25 of these components in each phase will preferably be optimized so that the refractive indices of the different phases match each other. The refractive index of the polymer alloy of the invention will depend on the reflective indices of the individual polymers and on the ratio of the individual polymers in the polymer alloy. Likewise, the refractive index of each phase will depend on the refractive
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indices of the individual polymers and on the ratio of the individual polymers within each phase.

The plasticizer, particularly if the plasticizer is mineral oil can easily migrate phase 5 to phase depending on the amount and nature of the individual polymers. This migration will affect the apparent refractive index of each phase. This migration of the plasticizer has to be taken into account in order to get the refractive indices of 10 the phases each composed of several components, to match. By measuring the haze of various formulations, the nature of the migration can be understood and used to develop the clearest formulations, i.e. formulations that create the best 15 clarity and lowest haze.

As taught herein above, the brittle polymer, the ductile polymer, and the rubbery polymer are preferably copolymers, i.e. consisting of more than one monomer. The refractive index of a copolymer 20 depends on the ratio of the individual monomers in the copolymer. In this instance, adjustments can be made to the refractive index of either phase by changing the copolymer ratio during polymerization, if feasible, or by blending like copolymers of 25 different ratios, if they are miscible. In this way, clear blends with a balance of toughness, stiffness and impact resistance can be obtained.

For the first embodiment of the invention, when the refractive indices of the different phases of 30 the polymer alloy match within + or - 0.005, the material will be transparent with a haze less than 5%. When the refractive indices of the different phases of the polymer alloy match within + or -

0.002, the material will have excellent clarity and a very low haze less than 3%, preferably less than 1.5%.

For the second embodiment, when the refractive indices of the different phases of the polymer alloy match within + or - 0.005, the material will be transparent with a haze less than 10%. When the refractive indices of the different phases match within + or - 0.002, the material will have a very low haze preferably between 1% and 4%.

The polymer alloy of the invention has a Notched IZOD impact strength ranging between about 1.0 to about 6.0, and preferably, ranging between about 2.0 and 4.5 foot pound per inch measured according to ASTM D-256.

The above is not intended to place any limitation on the order of mixing the polymers. It is not necessary to have a specific sequenced addition of polymers to the mixer.

In preparing the polymer alloy of the present invention, solution blending of the components is generally not useful, as it is difficult to find a common solvent for each polymer in the blend. As stated herein above, preferably, the plasticizer is blended with the brittle polymer prior to the brittle polymer being blended with the other polymers and the plasticizer resides in the brittle polymer when the brittle polymer is blended or mixed with the other polymers of the polymer alloy.

Typically, adequate mixing of the several polymers of the polymer alloy of the invention can be achieved by mechanical mixing in a suitable intensive mixer, preferably a single screw or twin

POLYMER ALLOY

screw extruder. If a single screw extruder is used, it should preferably be equipped with a modified mixing section to ensure adequate mixing of the components. Examples of common modified mixing sections are the Maddock mixing head and various designs from the Spirex Company such as the "Z-mixer".

Operation of an extruder to achieve this end is within the purview of a person skilled in the art.

10 For example, for an inch and a half extruder having an L to D ratio of about 24:1, the extruder is operated at from 30 to 150, preferably from 50 to 135, most preferably from 75 to 100, RPM. During such operation, the barrel temperature of the

15 extruder is in the range of from 190 to 240 °C., preferably from 200 to 220 °C.

Both the ductile polymer and the rubbery polymer may be individually fed to the extruder. Alternatively they may be mixed together and then

20 fed to the extruder, or mixed together and then extruded, and then chopped into pellets. The resulting pellets may then be extruded with the brittle polymer that contains the mineral oil. However, the components of the polymer alloy of the

25 present invention may also be dry-blended in, for example, a tumbler blender and then extruded. In an alternative procedure, the polymers may be fed directly to an extruder using loss-in-weight feeders for accurate composition control. As is common for

30 twin screw extrusion, some of the polymers and/or the plasticizer may be accurately metered into the extruder downstream of the main feed zone.

In a broad aspect of the invention, the brittle polymer will range from about 20 to 90 weight percent with a weight average molecular weight greater than 180,000 and comprising from 80 to 45
5 weight percent of one or more C₈₋₁₂ vinyl aromatic monomers (preferably, styrene) and from 20 to 55 weight percent of one or more C₁₋₆ alkyl esters of C₃₋₆ ethylenically unsaturated carboxylic acids (preferably, methyl methacrylate (MMA)) and from 0
10 to 5 weight % of one or more C₃₋₆ ethylenically unsaturated carboxylic acids or anhydrides; the rubbery polymer will range from about 0 to 60 weight percent; the ductile polymer will range from about 0 to about 80 weight percent; and the plasticizer will
15 be greater than 0.4 weight percent, based on the total weight of the polymer alloy.

The invention will be illustrated with reference to the following Examples, which should not be construed so as to limit the scope of the
20 present invention.

EXAMPLES

EXAMPLE 1

A summary of the blends of the polymer alloy of Embodiments 1 and 2 of the invention is shown in
25 Table 1. These blends contain styrene-methyl methacrylate (SMMA) as the brittle polymer in the amounts shown in Table 1.

TABLE 1

FORMULATION	Embodiment 1			Embodiment 2		
	Specific Range	Preferred Range	Broad Range	Specific Range	Preferred Range	Broad Range
% (wt.) brittle	50-55	40-70	20-80	55-65	50-70	20-80
% (wt.) ductile	45-50	30-60	20-80	25-35	20-40	0-60
% (wt.) rubbery	0	0-3	0-3	8-12	5-20	5-60
% (wt) oil	1.5	1-2	0.5-3.0	0.7-1.5	0.5-3.0	>0.5
SMMA (MW) (MMA wt%)	280,000 20-26	270,000- 300,000 20-35	>220,000 20-55	195,000- 270,000 30-35	190,000- 300,000 20-35	>180,000 20-55

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Two commercially available samples, Examples A and E, of polymer alloys of brittle polymer, ductile polymer, and rubbery polymers available from NOVA Chemicals, Inc., under the trademark ZYLAR® and 10 identified as prior art in Table 2 were injection molded into test pieces for conducting physical tests. These polymer alloys come within the composition ranges specified in U.S. Patent No. 5,294,677 that is owned by the assignee of the 15 present invention.

Test pieces for embodiments 1 and 2 containing the amounts/weights in the respective "Specific Range" columns in Table 1 were also prepared and tested. The mineral oil resided in the brittle 20 polymer. The components for embodiments 1 and 2 were in the form of pellets and were fed, in the desired amounts, to a twin screw extruder. Pre-drying of the resin components was not required. The extruder was operated at 75-100RPM and a temperature in the 25 range of 200 to 220°C. The mixture was extruded, chopped into pellets, and subsequently injection molded into a number of suitable specimens.

The following physical tests were then performed on both the ZYLAR® test specimens and the specimens of the invention:

5	Test	Identification
	Haze	ASTM D-1003
	Notched IZOD	ASTM D-256
	Tensile Properties	ASTM D-638
10	Elongation at Break	ASTM D-638

A comparison of the physical properties of polymer alloy of the ZYLAR® products with the polymer alloy of the invention is shown in Table 2.

- 15 For embodiment 2, both the measured result for the high rubber end of the Specific Range (i.e. 34 weight percent ductile and 10 weight percent rubbery) and expected results for the lower rubber limit (i.e. approximately 25 weight percent ductile
 20 and 8 weight percent rubbery), are given in Table 2. These are Example C and Example D, respectively.

TABLE 2

		Prior Art Example A	Invention Embodiment 1 (measured) Example B	Invention Embodiment 2 (measured) Example C	Invention Embodiment 2- Low Rubber (expected results) Example D	Prior Art Example E
Haze (0.1")	%	1.0	1.0	2.0	2.0	2.0
IZOD	Ft-lb/in	0.45	3.5	4.0	2.0	2.5
Falling Dart Peak Force	lb.	200	450	700	500	500
Tensile Strength	psi	5,200	3,500	3,500	4,800	4,200
Elongation	%	32	85	70	60	80
Tensile Modulus	psi	330,000	320,000	290,000	380,000	319,000

When Example A (prior art) is compared with Example B (invention) and when Example E (prior art) is compared with Example C (invention), it is observed that the polymer alloy of the invention has 5 an improved toughness (IZOD and Falling Dart Force) with no loss in clarity (Haze). Alternatively, when Example E (prior art) is compared with Example D (invention), it is observed that the polymer alloy of the invention having an improved stiffness, as 10 measured by Tensile Modulus, i.e. 319,000 (Example E) verses 380,000 (Example D) can be prepared with equivalent toughness i.e. a Falling Dart Peak Force of 500 psi for both Example E (prior art) and Example D (invention) and almost an equivalent IZOD 15 value i.e. 2.5 for Example E verses an IZOD value of 2.0 for Example D.

In general, as is evident from the test specimens in Table 2 above, the toughness of the specimens of the invention, as measured by both IZOD 20 impact strength and from Falling Dart Peak Force, show an improved balance between toughness, low haze and stiffness compared to the polymer alloys of the prior art.

EXAMPLE 2

25 A comparison specimen (No.1) and several polymer alloy specimens of the invention (Nos. 2-8) were prepared and were injection molded. Physical testing was performed similar to that explained in Example 1.

30 The specimens were comprised of the following components:

COMPONENT

Brittle Polymer:

5 A copolymer derived from SMMA
 (styrene- 70 weight percent and
 methyl methacrylate -30 weight
 percent). Experimental samples
 with different molecular
10 weights. Brittle polymer also
 contained the mineral oil (0 to
 3.5 weight percent) prior to
 blending of polymer alloy.

Ductile Polymer:

15 A tri-block copolymer derived
 from styrene (75 weight percent)
 and butadiene (25 weight
 percent), i.e. a styrene
 butadiene block copolymer.

Rubbery Polymer:

20 A tapered polymer derived from
 styrene (45 weight percent) and
 butadiene (55 weight percent),
 i.e. a styrene butadiene block
25 copolymer.

The amount of each component in the specimens
and the results of the physical testing are provided
in Table 3, wherein all units are in weight percent,
unless otherwise indicated.

30

TABLE 3

Run #	1	2	3	4	5	6	7	8
Sample ID								
Formulation								
% brittle (SMMA)	60	58.5	57.9	57.1	55.8	50.8	55.5	66.1
% ductile	28.4	28.4	28.4	31	33.5	37.5	35.6	27.6
% rubbery	11.6	11.6	11.6	10.4	9.3	10.4	8.3	5.6
% mineral oil	0	1.5	2.1	1.5	1.4	1.3	0.6	0.7
SMMA MW	194,000	194,000	254,000	194,000	194,000	194,000	194,000	194,000
Net butadiene % in alloy	13.5	13.5	13.5	13.5	13.5	15.0	13.5	10.0
Properties								
Haze (0.10") (%)	2.3	4.3	7.8	2.6	2.2	2.3	1.9	3.3
Melt (200/5) (g/10 min)	4.8	6.2	4.7	n/a	n/a	n/a	n/a	n/a
VICAT (°C)	98	95.3	94.8	95.8	96	93.4	N/a	n/a
IZOD (Notched)(ft-lb/in)	2.5	3.4	2.9	3.7	3.8	4.5	3.6	0.4
Tensile Strength (psi)	4150	3400	2800	3400	3470	3440	3990	4920
Elongation @fail (%)	78	64	50	66	70	70	78	52
Tensile Modulus (psi)	294,000	268,000	271,000	286,000	292,000	272,000	347,000	391,000
Falling Dart Impact Test								
Peak Energy (ft-lb)	7	23	33	23	14	32	9	5
Total Energy (ft-lb)	13.4	53	55	48	32	80	36	10
Peak Force (lb)	520	1000	1150	960	680	1130	580	470
(n/a-results not available)		(no break)	(no break)			(no break)	(no break)	(no break)

As is evident from these specimens 1 through 8,
 5 the addition of mineral oil and increasing the
 molecular weight of the brittle polymer gives a good
 balance of impact, tensile strength and tensile
 modulus, and acceptable low haze. A comparison of
 specimen 1 to specimen 2 shows that the addition of
 10 mineral oil increases toughness. A comparison of
 specimen 2 to specimen 4 demonstrates that adjusting
 the ratio of ductile and rubbery polymers can
 improve the refractive index match of the phases and
 reduce haze. Specimens 4 through 7, which are still
 15 within the scope of the invention, show that a
 reduction in the rubbery polymer component can
 produce a tough (IZOD) but still stiff (Tensile

Strength) product with acceptable low haze compared to specimen 1 that contains no mineral oil and that has a greater amount of rubbery polymer component. Even though specimen 8 has a low Notched IZOD value,
5 it still has good practical toughness (52% Elongation and 470 pounds Falling Dart Peak Force), as well as low haze and extremely high stiffness (390,000 psi Tensile Modulus).

This Example 2 therefore gives an indication as
10 to how the addition of mineral oil and a high molecular weight of the brittle polymer increase the toughening efficiency of the rubber phase (ductile and rubbery polymers).

15

EXAMPLE 3

A comparison specimen (No.1) and several polymer alloy specimens of the invention (Nos. 2-6) were prepared and injection molded. Physical testing was performed similar to that explained in
20 Example 1.

The specimens were comprised of the following components:

COMPONENT

25

Brittle Polymer:

30

A copolymer derived from SMMA (styrene- 79 weight percent and methyl methacrylate -21 weight percent). Experimental samples with different molecular weights. Brittle polymer also contained the mineral oil (0 to

5 weight percent) prior to blending of polymer alloy.

Ductile Polymer:

A tri-block copolymer derived from styrene (75 weight percent) and butadiene (25 weight percent), i.e. a styrene butadiene block copolymer. The copolymer is available commercially from Chevron-Phillips as K-Resin® KR03.

Each specimen was a blend of 50 weight percent brittle polymer and 50 weight percent ductile polymer. The results of the physical testing are provided in Table 4.

TABLE 4

Run No.		1	2	3	4	5	6
Molecular Weight	Mw of SMMA	220000	232300	264000	268500	290700	291000
Mineral Oil	(wt% in alloy)	0	1.41	1.37	2.31	2.3	1.64
Falling Dart Impact - Total Energy	ft-lbs	1.4	2.7	3.3	6.3	7.3	4.8
Falling Dart Impact - Peak Force	lbs	181.1	212.6	246.1	343.8	346.2	308.7
Notched IZOD	ft-lbs/in	0.38	0.43	0.89	4.96	5.28	3.35
Haze	%	1	3.8	1.8	2.9	3.5	2
VICAT	C	98.8	97.9	98	96.4	96.2	97.4
Melt Index	g/10min	4.35	3.93	3.77	4.27	4.0	3.57

As is evident from specimens 2 through 6, the addition of mineral oil and an increase in the molecular weight of the brittle polymer provide a significant increase in the toughness of the polymer alloy as measured by Notched IZOD and Falling Dart Impact Total Energy and Peak Force. In particular, Notched IZOD values well above 1 ft-lb/in were obtained for specimens 4-6, while the blend

(specimen 1) without mineral oil and a lower weight average molecular weight (220,000) obtained a Notched IZOD value of 0.38. Also for the specimens of the invention, the Falling Dart Impact Total 5 Energy values increased by almost an order of magnitude compared to that of specimen 1.

The haze can be further improved by adjusting the methyl methacrylate (MMA) content of brittle component in order to improve the refractive index 10 match.

INDUSTRIAL APPLICABILITY

The product of the present invention has improved low haze and improved transparency with 15 improved toughness and/or stiffness compared to the polymer alloys of the prior art. The polymer alloy of the present invention should be suitable in critical applications requiring clear and tough parts, for example, in the manufacture of appliance 20 housings, household accessories, and medical parts, particularly see-through, durable, and impact-resistant, medical components.

The invention is important in response to the growing trend in many markets to replace opaque 25 parts with clear components, and for aesthetic, design, visibility, and security reasons. The invention provides additional options at a lower cost and is easier to process (drop-in) with the customer's existing equipment.

30 While the present invention has been particularly set forth in terms of specific embodiments thereof, it will be understood in view of the instant disclosure that numerous variations

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upon the invention are now enabled yet reside within the scope of the invention.

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